| Page | Place | Error | It should be |
| :---: | :---: | :---: | :---: |
| 3 | paragraph Compliance | This means that the deformation is stiffness times load. | This means that the deformation is compliance times load. |
| 19 | formula 10.3 | $k_{\text {AC }}$ | $k_{B C}$ |
| 20 | $\begin{aligned} & \text { above figure } \\ & 10.14 \end{aligned}$ | a factor 1.5 | a factor 3 . |
| 23 | formula 10.14, line 2 | $=\int_{-\frac{1}{2} h^{2}}^{\frac{1}{2} h} \frac{1}{2} \frac{\sigma_{\max }^{2} \cdot 4 z^{2}}{E h^{2}} b L d z=\left[\frac{1}{2} \frac{\sigma_{\max }^{2} \cdot 4 z^{3}}{3 E h^{2}} b L\right]_{-\frac{1}{2} h}^{\frac{1}{2} h}$ | $=\int_{-\frac{1}{2} h}^{\frac{1}{2} h} \frac{1}{2} \frac{\sigma_{\max }^{2} \cdot 4 z^{2}}{E h^{2}} b L d z=\left[\frac{1}{2} \frac{\sigma_{\max }^{2} \cdot 4 z^{3}}{3 E h^{2}} b L\right]_{-\frac{1}{2} h}^{\frac{1}{2} h}$ |
| 26 | formula 10.25 | $\sigma(\rho, y, \varphi)=0 \quad \tau(\rho, y, \varphi)=\tau_{\max } \cdot \frac{2 z}{t}$ | $\sigma(x, y, z)=0 \quad \tau(x, y, z)=\tau_{\max } \cdot \frac{2 z}{t}$ |
| 27 | formula 10.26 | variable $h$ | variable $t$ |
| 28 | thickness in figure of thin tube | $t=q$ | $t=\frac{q}{2}$ |
| $\begin{aligned} & 30, \\ & 31 \end{aligned}$ | $\begin{aligned} & \text { equations } \\ & 10.29, \quad 10.30, \\ & 10.31,10.33 \end{aligned}$ | $\theta$ could have been expressed in $L$ and $h$ | $k_{\text {truss }}=\frac{E h^{3} L t}{4 L^{4}+4 L^{2} h^{2}+h^{4}}$ |
| 31 | equations 10.32, 10.34 | $h t^{3}$ | $h^{3} t$ |

Errata of Design Concepts Volume II, preliminary edition (August 2019)

| Page | Place | Error | It should be |
| :---: | :---: | :---: | :---: |
| 31 | line six from bottom of page | height to length ratio $h / L$ | length to height ratio $L / h$ |
| 31 | line two from bottom of page | stiffness almost the same as the stiffness of the sheet | that is not the case, it is not almost the same |
| 32 | figure 10.34 | stiffness of symmetrical truss should be as in figure: |  |
| 32 | equation 10.36 | equation of stiffness is wrong | $k_{\mathrm{truss} 2}=\frac{4 E L h^{3} t}{16 L^{4}+8 L^{2} h^{2}+h^{4}}$ |
| 33 | first sentence | stiffness almost the same as the stiffness of the sheet | that is not the case, it is not almost the same |
| 37 | formula 10.47 | $\left(12 a^{2}-12+4\right) \frac{E I}{L}$ | $\left(12 a^{2}-12 a+4\right) \frac{E I}{L}$ |
| 38 | formula 10.48, line 3 and 4 | $\left(12 a^{2}-12+4\right)$ | $\left(12 a^{2}-12 a+4\right)$ |


| Page | Place | Error | It should be |
| :--- | :--- | :--- | :--- |
| 38 | formula 10.49, <br> line 2 | $M(x)=\frac{\theta E I}{L}(4-6 a)+\frac{\theta E I}{L^{2}}(12 a-6) L a=\frac{\theta E I}{L}(6 a-2)$ | $M(L)=\frac{\theta E I}{L}(4-6 a)+\frac{\theta E I}{L^{2}}(12 a-6) L=\frac{\theta E I}{L}(6 a-2)$ |
| 45 | formula 10.68, <br> line 5 | $\beta=\frac{L_{I I}}{L_{I}}=\frac{1}{1-p}$ | $\beta=\frac{L_{I I}}{L_{I}}=\frac{p}{1-p}$ |
| 51 | equation 10.72 | $U=\ldots=\frac{1}{2} m \omega^{2} r^{2}(\sin (\omega t)+\cos (\omega t))^{2}=m \omega^{2} r^{2}$ | $U=\ldots=\frac{1}{2} m \omega^{2} r^{2}\left(\sin (\omega t)^{2}+\cos (\omega t)^{2}\right)=\frac{1}{2} m \omega^{2} r^{2}$ |

